

TEMPORARY SEDIMENT BASIN DESIGN SHEET

Computed by: BAG Date: 1/15/20
Checked by: DAS Date: 1/27/20

Project Name: Pxe
Basin No.: Sd3 #B-3
Total area draining to basin: 14.80 acres
Disturbed area to basin: 11.60 acres

Runoff Coefficient, c, for disturbed area to basin: <not used>
Runoff Coefficient, c, for offsite area to basin: <not used>

Avg. rainfall intensity for 2-yr storm in region (assume 10min Tc) I: <not used> in/hr
Avg. rainfall intensity for 25-yr storm in region (assume 10min Tc) I: <not used> in/hr

Volume

1. Compute minimum required storage volume (Vs)
Vs = 67 cy/ac * 14.80 acres = 992 cy or 26,773 cf
2. Compute volume of basin at clean-out (Vc)
Vs = 22 cy/ac * 14.80 acres = 326 cy or 8,791 cf

3. Determine elevation corresponding to minimum required storage volume, Vs
Min. riser crest elevation = 407.1 ft (from stage/storage relationship)
Design riser crest elevation = 407.1 ft (from actual riser crest elevation used)

4. Determine elevation corresponding to clean-out volume, Vc
Clean-out elevation = 405.5 ft (from stage/storage relationship)
Note: clean-out elevation shall be clearly marked on the riser or by a post near riser

5. Compute length of riser
Riser length = Design elevation of riser crest - Lowest elev of pipe at riser
Riser length = 407.1 ft - 402.95 ft = 4.2 ft

Stormwater Runoff

6. Compute peak discharge from a 2-yr, 24-hr storm event
Q2 = 30.3 cfs (taken from Hydrographs)
7. Compute peak discharge from 25-yr, 24-hr storm event
Q25 = 71.9 cfs (taken from Hydrographs)

Surface Area/Configuration Design

8. Compute minimum basin surface area (SAmin)
SAmin = 0.01 ac/cfs * Q2 = 0.303 ac = 43,560 sf/ac * 0.303 cfs = 13,177 sf

9. Check available area at riser crest
Available Area = 13,413 sf (determined by stage/storage relationship)
Available area >= SAmin? Yes X No

10. Compute required length to achieve 2:1 L:W ratio
Average width = 100 ft
Required length = 2 * average width = 200 ft
Lactual = 250 ft
2:1 L:W ratio satisfied? Yes X No
If no, refer to figure 6-22.2 for baffle designs. Note any required baffles on E&SC plan and include calculations and details for baffle(s).

Principal Spillway (ps)

11. Determine maximum principal spillway capacity Qmax = Q2 = 30.25 cfs
12. Compute the vertical distance between the centerline of the outlet pipe and the emerg. spillway crest (H)
H = 4.7 ft
13. Compute the total pipe length of the principal spillway, L, using Figure 6-22.3
L = [A - (B+C)/2][Zu+Zd] + T + E
A = 409.00, B = 403.18, C = 402.95, T = 5.00, E = 0.00
Lreq = 38 ft, Lactual = 45 ft

14. Determine diameter of principal spillway (Dps) and flow through principal spillway (Q) from Table 6-22.1 using H and Qmax
Dps = 36 (double 36" culver) Q = 145.00 cfs (actual value from 6-22.1)
Note: Table 6-22.1 is for CMP, this is RCP, see equation 2.3.4 in GSMM for flow rate

15. Compute actual flow through principal spillway, using Table 6-22.1 to determine the correction factor for pipe length, L
Qps = Q * correction factor = 145.00 * 1.00 (RCP, not CMP)
Qps = 145.00 cfs > Q25 = 71.88

Therefore, Principal Spillway is adequate to handle the 25-year storm an emergency spillway is for redundancy only

16. Compute riser diameter (Dr)
Dr >= 1.5 * Dps = 54 in
Dr = 54 in

17. Compute trash rack diameter (Dt)
Dt >= 1.4 * Dr = 75.6 in
Dt = 80 in

18. Determine minimum distance between the riser crest and the emergency spillway crest, h, using table 6-22.2, Dr, and Qps
h = 2.0 ft
Actual Q = 123.9 < 145.00 (Qps)

Concrete Riser Base Design

19. Determine the volume of concrete per vertical foot of riser height needed from Table 6-22.3 to prevent floatation.
Required volume of concrete per vertical foot = 13.9 cf/ft
20. Compute total volume of concrete required
Total required volume of concrete = Required volume per vertical foot * Riser Length = 13.9 cf/ft * 4.2 ft = 57.99 cf
21. Assume base thickness (usually 18") (B).
B = 18 in = 1.5 ft
22. Compute required surface area
Required surface area = Total volume required / B = 57.99 cf / 1.5 ft = 38.5 sf
23. Compute riser base length (l) and width (w) (assume square base), (AKA "B" and "C" in Sd3 cross section)
l = w = (required SA)^{0.5} = 38.5 sf^{0.5} = 6.20 ft = 12in/ft * 6.20 ft = 74 in

Anti-Seep Collar Design

24. Determine if anti-seep collar is required. If yes to any of the following conditions, a collar is required:
The settled height of the dam is greater than 15 feet.
The principal spillway diameter (Dps) is smooth pipe larger than 8".
The principal spillway diameter (Dps) is corrugated metal pipe larger than 12".

25. Determine if anti-seep collar is required.
X 18-inch projection (for heads (H) less than or equal to 10 feet).
24-inch projection (for heads (H) greater than 10 feet).

Emergency Spillway (es)

No Spillway Provided. 100yr storm contained within Sd3
26. Compute minimum capacity of emergency spillway (Qes)
Qes = Q25 - Qps = 71.88 - 145.00 = -73.12 cfs
Therefore, Size for Q25 (redundancy) Qes = 71.88 cfs

27. Determine stage (Hp), bottom width (b), velocity (V), and minimum exit slope (S) using Table 6-22.4 and Qes.
Hp = 5 ft, b = 5 ft, V = 5 fps, S = 5%

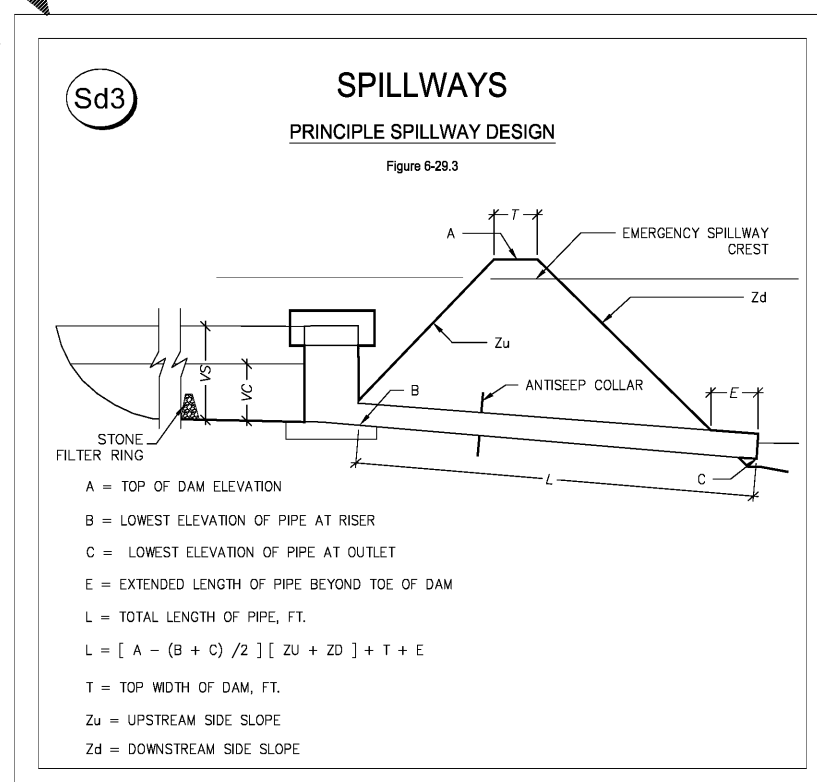
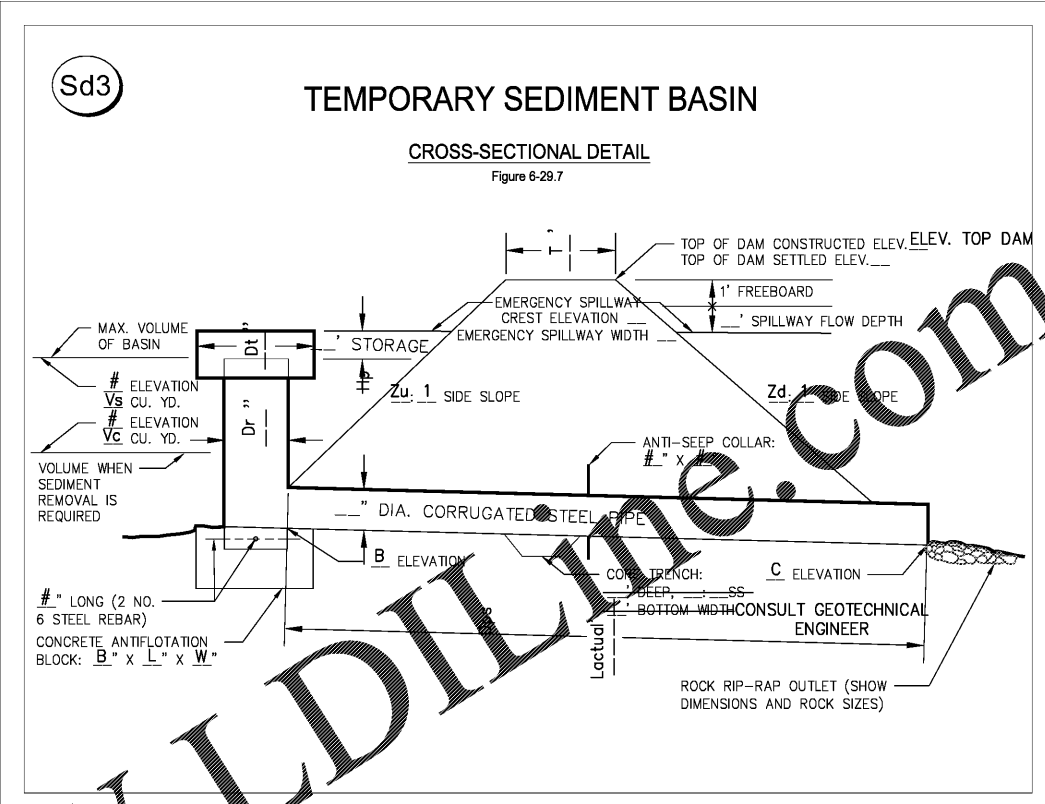
28. Actual entrance channel slope, Se = 5%
29. Actual exit channel slope, So = 5%

Note: If So is steeper than 5 (from Table 6-22.4), then the velocity in the exit channel exit channel will increase.
a) Calculate the new exit velocity (Vo)
Vo = V(So/S)^{0.5} = 5 * (5/5)^{0.5} = 5 fps; therefore, #DIV/0!

Refer to Channel Stabilization (Ch) to determine proper lining for emerg. spillway
Grass Rip-rap X Concrete
Therefore, use: Rip-Rap

Design Elevations

30. Riser crest elevation = 407.1 ft
31. Compute minimum emergency spillway crest elevation
Min. emergency spillway crest = riser crest elevation + h = 407.1 + 4.7 = 411.8 ft
Min. emergency spillway crest = 409.1 ft
Design emergency spillway crest = 409.1 ft
32. Determine design high water elevation
Design high water elevation = Emerg. spillway crest + Stage elevation (Hp) = 409.1 + 0.0 = 409.1 ft
Design high water elev. = 409.1 ft
33. Determine elevation of top of dam
Elevation of top of dam = Design high water elevation + 1 ft freeboard = 409.1 + 1 = 410.1 ft
Elevation of top of dam = 410.1 ft
Actual Elevation of top of dam = 410.0 ft (existing driveway)



Sd3 CALCULATIONS

BASIN I.D.	RISER BOX & PRINCIPLE SPILLWAY			EMERGENCY SPILLWAY				DAM				SEDIMENT STORAGE											
	Dps (in)	Dr (in)	Dt (in)	Riser Elev.	Length, L (ft)	Inv Elev. (Up)	Inv Elev. (Down)	Storage, h (ft)	AF Block	Crest Elev	Bottom Width (ft)	Hp (ft)	Lining	T (ft)	SS1 (H:1V)	SS2 (H:1V)	Freeboard (ft)	Top of Dam Elev.	Drainage Area (ac)	Maximum Vs Elev.	Volume, Vs (cf)	Clean-Out Vc Elev.	Volume, Vc (cf)
1	36	54	80	407.1	45	403.2	403.0	2	A (in) 18, B (in) 74, C (in) 74	409.1	0	0	Rip-Rap	5.00	2.50	3.00	1.0	410.0	14.80	407.1	26,773	405.5	8,791



REVISIONS			
No.	Description	Date	By

Project Name: APRON EXPANSION PROJECT

Sheet Name: ES&PCP DETAILS NO. 2

GDOT Project Number: APXXX-XXXX-XX(XXX) Holt Project Number: GAxxxx-xx

Designer: W. MGNAMARA Technician: B. GARROW Checked by: D. SKURKY

CAD File: C:\07 Erosion Details.dwg Submittal / Issue Date: FEBRUARY, 2020

Plotted: Feb 17, 2020 - 8:21am by George Sumas Drawing Number: CE 5.02

Scale: N.T.S.